

Multi-Disciplinary Design Optimization for Relative Navigation in Non-cooperative Rendezvous

Clément Rappasse
Cranfield University
College Road
MK43 0AL, Cranfield, United Kingdom
clement.rappasse@gmail.com

Baptiste Agez
ONERA - The French Aerospace Lab
6 Chemin de la Vauve aux Granges
91120 Palaiseau, France
baptiste.agez@onera.fr

Nicolas Merlinge
ONERA - The French Aerospace Lab
6 Chemin de la Vauve aux Granges
91120 Palaiseau, France
nicolas.merlinge@onera.fr

Leonard Felicetti
Cranfield University
College Road
MK43 0AL, Cranfield, United Kingdom
Leonard.Felicetti@cranfield.ac.uk

Abstract—On-orbit applications, such as active debris removal, satellite refueling, maintenance and satellite health diagnosis require the ability for low-cost spacecraft to closely inspect other orbital objects in a non-cooperative manner. During this kind of mission, the relative navigation process becomes of critical importance for guaranteeing safe and collision-free proximity operations and maneuvers. The selection of relative navigation sensors appears being a critical task as it might drive the design choices in other subsystems (e.g., Attitude and orbit control system (AOCS), payload, power supply). This paper aims at studying the application of a Multidisciplinary Design Optimization (MDO) method to the design of AOCS and Navigation subsystems under small satellite constraints. The proposed MDO process is based on the optimization of navigation performance and mass reduction while respecting volume and power constraints for orbital close rendezvous. The navigation chain, including sensor simulation and navigation filter is simulated and integrated into the design cost function. The proposed MDO process based on a Genetic Algorithm (GA) and on an Extended Kalman Filter (EKF) aims at simplifying satellite design by determining a set of optimal admissible sensor combinations despite contradictory objectives on navigation and payload accuracy, mass reduction, power consumption and volume. Possible key advantages of the inclusion of the relative navigation subsystem within MDO process are the reduction of the design process time, the automation and optimization of the navigation architecture while respecting volume and power constraints of small satellites. A demonstration of the effectiveness of the proposed MDO method is provided on the benchmark of AVANTI mission.

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1. INTRODUCTION

Non-cooperative rendezvous represents one of the key assets that can enable active debris removal operations and on-orbit servicing missions. The close approach and docking to a non-cooperative target is indeed the first and necessary step of a sequence of possible operations that future mission can perform for de-orbiting dangerous pieces of debris, for carrying out health diagnoses, repair and refuel satellites in orbit [1] [2].

Compared to cooperative rendezvous, where both the chasing and target satellite cooperatively share information about their mutual positions, the relative navigation task during non-cooperative rendezvous appears to be more complex and critical, because it needs to be carried out only by the chaser satellite only. Only a few non-cooperative rendezvous were performed to date, mainly because of the risk of collisions and the technical performance of space-qualified relative navigation sensors [3] [4]. Such kind of issues become even more challenging when the non-cooperative rendezvous tasks need to be accomplished by small-sized satellites, where the selection of the relative navigation hardware becomes the key driver for the overall spacecraft and mission design. Indeed, the selection of a fairly accurate combination of sensors (e.g. cameras, LIDARs etc.) might contribute to the mission success or even enhance the performance of the mission, but in some cases the range of possible options can be limited by volume, power or even cost constraints. Such a selection might also have important consequences on the definition of the different architectures and components for other subsystems (e.g. Attitude and Orbit Control System (AOCS), payload, power subsystem etc.) and in some cases an optimal global design is not possible, due to concurrent needs and requirements imposed by the different subsystems and, consequently, only a compromise can be achieved.

The process of finding a good initial guess for the baseline architecture of the mission is difficult and somehow based on the experience of the system engineers who, in some cases, might not be aware of the latest state-of-art technology available on the market. It appears then evident that a tool addressing these initial challenges, by taking into account the multidisciplinary nature of the design process, might have tangible benefits in terms of reduction of the design process time, automation and optimization of the selection of specific key hardware, especially when the project is carried out in an agile design framework.

The utilization of Multidisciplinary Design Optimization

(MDO) tools during the mission and spacecraft design has gained an increased interest from both industrial and scientific applications in the past decades. Providing a trade-off support while accounting for decision-maker preferences has made MDO a critical tool when dealing with high-complexity design problems. It was first introduced and defined in late 1980s by J. Sobieski [5] as "an emerging new engineering discipline" allowing the optimization of a system whose subsystems and physical phenomena are interrelated. In literature, many studies mention the use of MDO for designing aerospace vehicles. N. Bérend and S. Bertrand [6] developed a MDO methodology to optimize the mass of each discipline for aerobraking orbital transfer vehicles. W. Wu et al. [7] proposed to include a parametric finite element model in the structure discipline of an MDO model to improve the fidelity of the analysis model and therefore optimize the design of the satellite. X. H. Wang et al. [8] compared three MDO methods (Collaborative Optimisation, All-at-Once and Multi-disciplinary Feasible Method) to optimize the performance of an Earth observation satellite. J.T. Hwang et al. [9] developed a large-scale multidisciplinary design optimization involving seven disciplines and over 25,000 design variables for a small satellite. Recently, R. Shi et al. [10], whose objective was to reduce the total mass of an all-electric GEO satellite, proposed a surrogate assisted MDO framework involving most of the sub-systems. S. Berrezzoug et al. [11] exposed the use of MDO for the design of a geostationary communication satellite. The application of the MDO to the design of small satellites performing non-cooperative rendezvous seems, to the knowledge of the authors, unexplored but worth further investigations.

The goal of this paper is to present a MDO process that can satisfy the specific objectives and multidisciplinary needs of the design of several satellite sub-systems for non-cooperative rendezvous. Specifically, a particular attention will be given to the selection process addressing the relative navigation tasks, selecting the optimal combination of navigation sensors (IMU, LIDAR, Star tracker etc.) which feed a standard relative navigation algorithm (e.g. Extended Kalman Filter) with the aim of having a complete and accurate estimation of the relative position, attitude and velocity of the chaser satellite with respect to the target in a standard rendezvous scenario. Key performance index, such as the accuracy of the estimation (i.e. covariance matrix) can be indeed paired with classical system design parameters and included into a cost function in order to enable a more comprehensive and navigation-focused trade-off among the different options. A genetic algorithm is used to select and optimize the combination of sensors from a database of the state-of-art navigation technology alongside with a standardized definition of the key error models for each typology of sensors. Constraints on power, cost and volume, as well as inter-relations with other subsystems (such as AOCS, power etc) are taken into account during the process.

The remaining structure of the article is as follows. In Section 2, a formulation of a suitable MDO problem is proposed, for sizing and selecting components of AOCS, GNC and payloads for performing rendezvous. The section also defines the main coordinate frames and parameters used during the formulation as well as outlines the Kalman Filter that has been selected for the navigation task. Section 3 presents the MDO process that solves the problem by taking into account requirements and constraints imposed by other subsystems and their interactions with the relative navigation components. A database of the main characteristics of commercial-off-the-shelf components is then presented

in Section 4, alongside with their error models. Section 5 presents the resulting optimal GNC configurations obtained by the application of proposed MDO algorithm to the test case scenario of the AVANTI mission. The performance analysis and numerical simulations with this section will show the consistency of the selected configuration as well as demonstrate the validity of the proposed MDO methodology. Finally, Section 6 summarizes the main findings, conclusions and future works of the authors in this area.

2. PROBLEM STATEMENT

The present work proposes a methodology to automatize and optimize the GNC design for a satellite that needs to perform a non-cooperative rendezvous within its mission. The considered model accounts for:

- AOCS actuators (e.g. thrusters, reaction wheels, etc.);
- AOCS and relative navigation sensors (e.g. IMUs, LIDARs, Star-trackers);
- A relative navigation algorithm (e.g. Extended Kalman Filter) providing a complete navigation solution (relative position and velocity with respect to the target and absolute orientation of the chaser);
- A payload whose performance is dependent from the AOCS and/or navigation chain. Without loss of generality, we consider a passive sensor pointing towards the target (e.g. a camera) and aiming to measure distances on the surface of the target.

The following subsections provide a baseline framework in order to define the considered rendezvous scenario (Section 2-1) and the adopted relative navigation algorithm (Section 2-2) that then concur to the formulation and specification the MDO problem for the design of a spacecraft performing non-cooperative rendezvous (Section 2-3).

1. Non-cooperative rendezvous scenario

Figure 1 shows a typical non-cooperative rendezvous scenario where the chaser satellite (denoted with the letter B) is supposed to approach and rendezvous to the target satellite (denoted with the letter A). The chaser is therefore required to estimate its relative position through the use of its sensors (e.g. IMU, star sensor, LIDAR) and consequently perform a rendezvous maneuver by using the on-board actuators (e.g. thrusters and reaction wheels). Three different reference frames are defined: namely, $[\hat{x}, \hat{y}, \hat{z}]$ shapes the Earth Central Inertial frame (ECI) frame, $[\hat{r}_x, \hat{r}_y, \hat{r}_z]$ describes the Local Vertical Local Horizontal (LVLH) frame associated to the target and $[\hat{b}_x, \hat{b}_y, \hat{b}_z]$ is the body frame associated to the chaser B. The positions of the two satellites are defined by \mathbf{r}_A and \mathbf{r}_B in the ECI frame, respectively and, $\delta\mathbf{r}$ represents the relative position of the chaser with respect to the target. The latter is usually defined with the components taken with respect to the LVLH frame.

The variables characterizing the chaser satellite with respect to the target satellite are gathered in the state vector \mathbf{x} described in Eq. (1): $\delta\mathbf{r}$ and $\delta\dot{\mathbf{r}}$ define the relative position and velocity in the LVLH frame of the target satellite, the quaternion \mathbf{q} and the angular velocity $\boldsymbol{\omega}$ describes the attitude of the chaser satellite in the body frame.

$$\mathbf{x} = [\delta\mathbf{r} \quad \delta\dot{\mathbf{r}} \quad \mathbf{q} \quad \boldsymbol{\omega}]^T \quad (1)$$

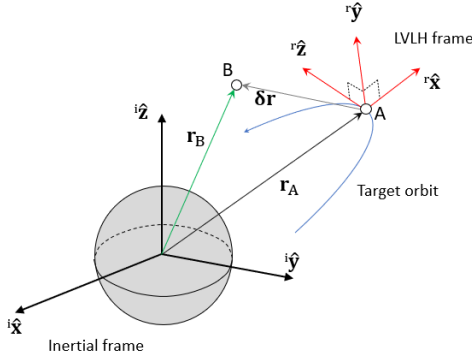


Figure 1: Position of chaser B relative to target A

To control the relative position, the relative velocity and the attitude of the chaser satellite, a control command vector \mathbf{u} defined in Eq. (2) where \mathbf{u}_a provides the accelerations by the thrusters in the LVLH frame and \mathbf{u}_t , the torques in the body frame.

$$\mathbf{u} = [\mathbf{u}_a^T \quad \mathbf{u}_t^T]^T \quad (2)$$

The navigation problem consists of estimating the system's state $\mathbf{x} \in \mathbb{R}^d$ from a series of measurements $\mathbf{x} \in \mathbb{R}^{d_m}$. The estimation scheme can be defined as an iterative stochastic process made of the state \mathbf{x} and the measurements \mathbf{y} . The state evolution is described by a dynamical model f :

$$\mathbf{x}_k = f(\mathbf{x}_{k-1}, \mathbf{u}_k) + \mathbf{w}_k \quad (3)$$

where \mathbf{w}_k represents the process noise, and the measurements are linked to the state by an observation model :

$$\mathbf{y}_k = h(\mathbf{x}_k) + \mathbf{v}_k \quad (4)$$

where \mathbf{v}_k represents the observation noise.

2. Extended Kalman Filter

Relative and absolute navigation can be performed on-board by a Kalman Filter [12]. The Kalman Filter iteratively fuses the information provided by an *a priori* defined evolution model of the system with onboard measurements to obtain an estimation of the relative kinematic status of the chaser with respect to the target. The first step of the process consists in predicting the state vector (see sub-section 2-1) propagating the physical model. The second step updates the predicted state using the measurements. Figure 2 summarizes the steps and variables introduced in the Kalman Filter.

Time update—This step consists in predicting each variable of the state vector from time-step k using physical models to obtain a predicted state $\hat{\mathbf{x}}_{k|k-1}$. For example, in the case of close orbital rendezvous, the prediction of relative position and velocity is based on the Clohessy-Wiltshire equations [13]. The predicted covariance matrix $\hat{\mathbf{P}}_{k|k-1}$ is obtained from the dynamical Jacobian matrix, the prior covariance matrix $\hat{\mathbf{P}}_{k-1}$ and the process noise covariance \mathbf{Q}_k that reflects approximations made to solve the equations as linearization.

\mathbf{F} is obtained by $\mathbf{F} = \frac{\partial f}{\partial \mathbf{x}} \Big|_{\mathbf{x}=\mathbf{x}_k}$.

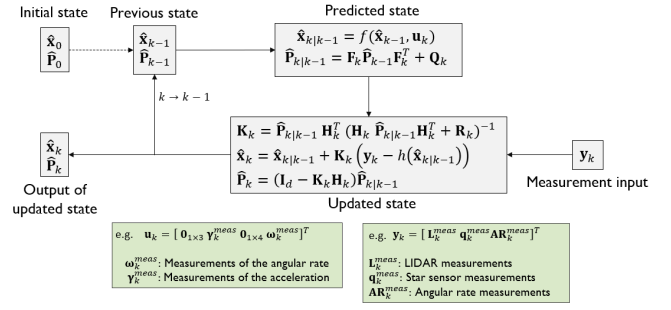


Figure 2: Extended Kalman Filter flowchart

Measurement update—Once the state vector is predicted by the model, values are updated using the measurements \mathbf{y}_k . \mathbf{H}_k is the observation Jacobian matrix obtained by $\mathbf{H}_k = \frac{\partial h}{\partial \mathbf{x}} \Big|_{\mathbf{x}=\mathbf{x}_k}$.

All variables of the state vector are not necessarily measured. In this simulation, the relative position, the quaternion and the angular rate are measured by a LIDAR and a star sensor. The Kalman gain \mathbf{K}_k is also introduced in this step. It weights the importance of the measurements and of the model. \mathbf{R}_k is the measurement covariance matrix. In practice, \mathbf{R}_k is defined from the sensors performance characteristics and must be diagonal and positive definite.

To propagate the Kalman Filter, the initial state vector $\hat{\mathbf{x}}_0$ and the initial estimate covariance matrix $\hat{\mathbf{P}}_0$ are defined as initial conditions, according to the considered scenario.

Application to relative navigation—Generally, a navigation system relies on IMU iterative integration. However, the IMU navigation solution drifts because of gyrometric and accelerometric sensing errors. Therefore, IMU needs to be hybridized with additional sensors to correct the navigation solution. The whole navigation performance depends both on IMU accuracy and hybridization sensors accuracy. In the case of a relative navigation filtering scheme, IMU performance has an impact on covariance prediction (*Time update*) via the covariance matrix \mathbf{Q}_k . The hybridization sensors have an impact on the correction step via the covariance matrix \mathbf{R}_k used to compute the Kalman gain \mathbf{K}_k (*Measurement update*).

3. Multidisciplinary Design Optimization

Usually, the search for an optimal solution in engineering problems is performed thanks to gradient based methods, especially when the number of variables or functions is easy to deal with. Most complex problems, however, such as satellite design, requires suitable tools, capable of operating in the presence of a considerable number of variables and couplings [14].

Those tools, mostly used in the field of design optimization, are called stochastic methods. As opposed to deterministic methods, stochastic methods randomly search in the design space, free from specific rule or initial guesses. In the MDO process, this stochastic aspect lies upon the choice of the algorithm.

Considering their ease of use, Evolutionary Algorithms (EA) such as Genetic Algorithms (GA) are most of the time chosen [15]. Inspired by biological evolution, EA mathematically reproduces the natural mechanisms of mutation, recombination and selection over a set of individuals forming a population [16]. Selection operator gives the fittest solutions the highest

probability to be in the next generation; recombination (or crossover) creates a new solution by mixing two solutions from the previous generation; and eventually mutation can randomly modify some solutions. The flow chart of such algorithm [17] is given in Figure 3.

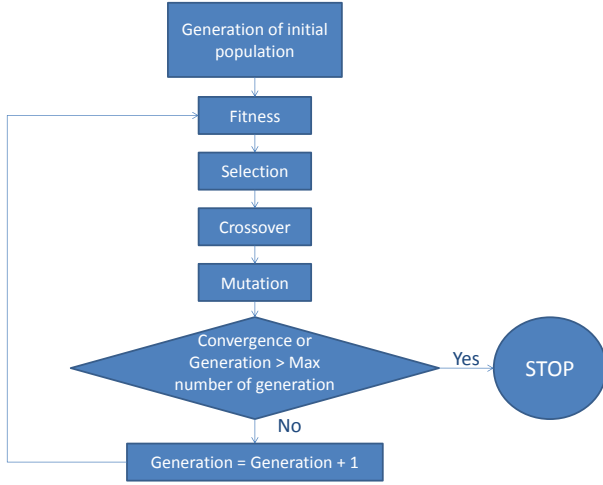


Figure 3: General flow chart of a genetic algorithm.

In MDO terms, GA can deal with large design space, being able to handle optimization problems with many local optima. This capacity, along with the ease of use and adequation to discrete design variables [15], makes GA the chosen algorithm for the present optimization problem.

Inside the MDO process, the algorithm deals with the design variables, which constitute the population of individuals. At each iteration, the fitness of every candidate is evaluated thanks to mathematical models. The fitness is related to an objective function, in which the user puts different criteria of his choice, and to constraints, if any, that the solution must respect.

A MDO problem for a single objective can thus be mathematically written as follow [18]:

$$\mathbf{X}^* = \underset{\mathbf{X} \in \Omega \leq \bar{\mathbf{X}}}{\operatorname{argmin}} F(\mathbf{X}) \quad (5)$$

where $F(\mathbf{X})$ is the objective function, $G(\mathbf{X})$ is the constraint function and \mathbf{X} the vector of design variables which can move freely inside the design space Ω .

In practice, the process can be divided into several sequential steps :

- Definition and selection of the design variables, which have the major impact on design;
- Evaluation of design for a set a variables thanks to the mathematical model of the system;
- Computation of the objective function for this specific design;
- Iterations on variables via an optimization algorithm to get the best design configuration.

Several approaches exist and use different architectures to tackle the problem, including MDF (Multi-Disciplinary Feasible), CO (Collaborative Optimization), AAO (All-At-

Once), BLISS (Bi-Level Integrated Synthesis), CSSO (Concurrent Subspace Optimization) among others. Their major difference lies in their way of proceeding and organizing the different parts (variables, objectives, constraints) of the process. For instance, they can be single or multi-level, meaning that they would perform subsystem's optimization before proceeding to system-level optimization. Interested reader can refer to [19] for more information.

In this study, two main objectives are included in the objective function: minimizing the mass and maximizing the performances (i.e. minimizing their errors) of the satellite embedded sensors. Both are the results of Multidisciplinary Analysis (MDA) of several satellite's subsystems, described in section 3-2. The constraints associated to the problem are the volume occupied by the embedded devices (sensors and actuators) and their power consumption. A single level All-at-Once (AAO) framework is used to formulate our problem :

$$\begin{aligned} \mathbf{X}^* = \underset{\mathbf{X} \in \Omega}{\operatorname{argmin}} \quad & F[M(\mathbf{X}), \sigma_p(\mathbf{X}), \sigma_v(\mathbf{X}), \sigma_q(\mathbf{X}), \boldsymbol{\varepsilon}(\mathbf{X})] \\ & V(\mathbf{X}) - \bar{V} \leq 0 \\ & P(\mathbf{X}) - \bar{P} \leq 0 \end{aligned} \quad (6)$$

where $\mathbf{X} \in \mathbb{N}^N$ is a vector of discrete variables pointing towards a combination of N embedded devices (e.g. navigation sensors, thrusters, payload sensors), $V(\mathbf{X})$ is the total volume occupied by the selected devices, \bar{V} is the maximum admissible volume, $P(\mathbf{X})$ is the total power consumption for the selected devices, \bar{P} is the maximum admissible power, $\Omega \subset \mathbb{N}^N$ is the design space (i.e. the list of all possible device combinations), $M(\mathbf{X})$ is the total mass of the selected devices, $\sigma_p(\mathbf{X})$, $\sigma_v(\mathbf{X})$, and $\sigma_q(\mathbf{X})$ are respectively performance indicators for navigation (relative position, relative velocity, and absolute attitude) and $\boldsymbol{\varepsilon}(\mathbf{X})$ contains some performance indicator about the payload in terms of error (e.g. position and velocity error estimation of a point located on the surface of the target).

In the specific case of a device combination involving: one IMU, one star tracker (ST), one LIDAR (L), a payload (P), one type of thrusters (TH) and one type of reaction wheels (RW), the design vector is defined as:

$$\mathbf{X} = [X_{IMU} \ X_{ST} \ X_L \ X_P \ X_{TH} \ X_{RW}]^T \quad (7)$$

3. METHODOLOGY

This section presents the proposed MDO methodology to solve the Problem (Eq. (6)). An overview of the MDO process is first given. Then, the modeling of each subsystem is detailed in terms of cost function and constraint and represented in Figure 4.

1. MDO methodology

MDO relies on an optimization algorithm that determines the optimal device configuration (i.e., navigation sensors, payload and actuators) given design constraints (e.g., volume, power). Since the considered design variables are discrete choices of COTS sensors, the optimization algorithm must handle discrete optimization space. As mentioned previously, GA is selected: this type of optimization algorithm iterates on a population of candidate configurations and aims to achieve a consensus. A convergence is met when a consensus is

achieved among the population of candidate solutions. A given candidate solution is evaluated by cost functions that are developed in the following sections.

For a given device configuration, the sensor measurements \mathbf{y}_k are simulated from a reference trajectory and processed by the navigation filter. Scalar performance criteria are defined to quantify the navigation performance at a given time-step k_e of the scenario. Actuators and payload performance requirements are also modeled, depending on sensors and navigation performance. Finally, structural and design characteristics are evaluated (e.g. sum of all devices mass, volume and power consumption). This scheme is characterized by strongly nonlinear and interdependent couplings between involved subsystems, which motivates the use of an optimization algorithm.

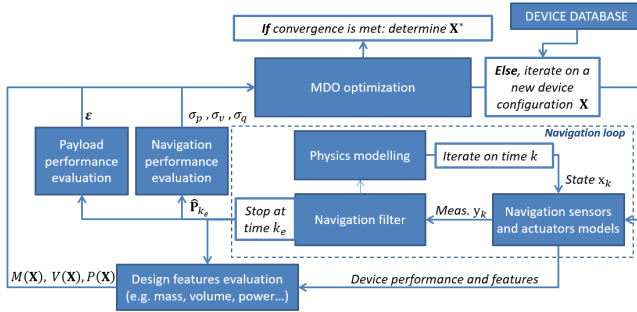


Figure 4: Overview of the proposed MDO methodology: a discrete optimization algorithm evaluates the cost and constraints of Problem (Eq. (6)) by running a temporal loop simulating the whole navigation process. The MDO process aims to determine the best sensor configuration \mathbf{X}^* .

2. Subsystems modeling

This section details the modeling of all considered subsystems of Problem (6). The following assumptions are made:

- The nominal trajectory of the chaser is a constraint given by a prior mission preparation process and is not a design variable;
- The flight avionics calculator is not considered as a design variable;
- Each device is dedicated to one specific task;
- The total available volume for all the devices is a constraint;
- The power supply system is fixed and constrains the total energy available on-board;
- The relative positioning of the devices in the body frame is not considered.

AOCS and GNC performance—The attitude and orbit control subsystem is directly related to the guidance and navigation subsystem. The choice of sensors is the key part of the MDO process, and is thus subject to higher fidelity than the other models.

A database of COTS sensors (IMU, LIDAR, Star Tracker), described in Section 4, has been built and provides figures for the sensors and actuators: expected performance, mass, volume, and power consumption. The relative navigation algorithm (e.g., the Extended Kalman Filter presented in Section 2-2) provides a complete navigation solution (relative position and velocity with respect to the target and absolute orientation of the chaser). The navigation performances indicators are defined by the spectral radius $\rho(\bullet)$ of the filter's covariance sub-matrix for each sub-state vector (e.g. position,

velocity, attitude) at an *a priori* defined time of evaluation k_e (e.g. at final time):

$$\begin{aligned}\sigma_p(\mathbf{X}) &\triangleq \rho(\hat{\mathbf{P}}_{k_e}^p) \\ \sigma_v(\mathbf{X}) &\triangleq \rho(\hat{\mathbf{P}}_{k_e}^v) \\ \sigma_q(\mathbf{X}) &\triangleq \rho(\hat{\mathbf{P}}_{k_e}^q)\end{aligned}\quad (8)$$

where $\hat{\mathbf{P}}_{k_e}^p$, $\hat{\mathbf{P}}_{k_e}^v$, and $\hat{\mathbf{P}}_{k_e}^q$ are the position, velocity and attitude sub-matrices of the filter's covariance $\hat{\mathbf{P}}_{k_e}$. Note that this definition is not dependent of the specific navigation algorithm and can be applied to other recursive filters.

To complete the design of the AOCS subsystem, actuators must also be considered. Reaction wheels, combined with small thrusters, are selected. This set up is often used for 3-axis control spacecraft [20]. Thrusters are necessary provide small orbit corrections, while wheels are used for orientation, attitude perturbations and relative maneuvers.

As for sensors, a database of reaction wheels and thrusters for small satellites applications was built, that outputs mass, power consumption, and performance for each device, namely torque capacity for the wheels and thrust and Isp for thrusters. In the frame of the MDO process, actuators come into play when sensors have been selected at each evaluation i . Once the sensors' performance and their respective accuracies are known, it is then possible to compute the requirement in terms of Δv and torque.

In this paper, the function of thrusters is dual. They desaturate the wheels and provide motion for orbit corrections. These corrections, considered for Δv calculations, are based on the relative position and velocity uncertainties obtained from the sensors and the navigation filter performance. Specific Impulse requirements are then addressed thanks to Tsolkovsky's equation :

$$Isp = \frac{\Delta v}{\ln\left(\frac{m_{init}}{m_{final}}\right)g_0} \quad (9)$$

where $g_0 = 9.81 \text{ m/s}^2$ is the gravitational constant, m_{init} the initial mass (before thrust) and m_{final} the final mass. Δv must account for both velocity and position errors: considering a distance correction of σ_p to achieve within a period t_{man} , two maneuvers (one for catching back the missing distance, one for slowing down back to previous velocity) are required with total absolute value $2\sigma_p$, which yields $\Delta v = \sigma_v + \frac{\sigma_p}{t_{man}}$.

On the other hand, momentum dumping requires a thrust force F that can be determined by the following formula [20]:

$$F = \frac{h_w}{L t_{burn}} \quad (10)$$

with h_w the stored momentum, t_{burn} the burn time and L the moment arm.

The same process can be applied for the wheels. The values of the uncertainties on pitch/yaw and roll orientations resulting from sensors' performance are taken as inputs to determine the torque capacity of the wheel necessary to account

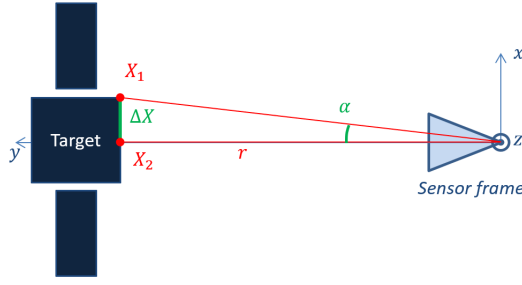


Figure 5: Payload relative sensor scheme. The range r is assumed to be significantly larger than the distance ΔX between two points of the target.

for those perturbations. The necessary slewing torque is [20]:

$$T = 4\theta \frac{I}{t_{spin}^2} \quad (11)$$

with I the inertia of the satellite, t_{spin} the spinning period, and θ the slew angle required. In our case, θ constitutes the maximum uncertainty angle among the three Euler angles obtained from the star tracker.

The second characteristic of wheels is their angular momentum capacity, which allows a wheel to store the acquired momentum. This parameter is obtained with the torque T and the acquisition time t_{acq} [20]:

$$h_w = \frac{2Tt_{acq}}{\sqrt{2}} \quad (12)$$

Payload—In addition to the AOCS and GNC sensor chain, a payload device is considered. The payload performance may be coupled with AOCS and/or navigation sensors. In this work, we consider a relative passive sensor pointing towards the target (e.g. a camera) and aiming to determine:

- Distances on the surface of the target;
- Velocity of points on the surface of the target (e.g. if the target is spinning).

The payload is assumed to measure an angle $\alpha \in [-\pi, \pi]$ between the Lines Of Sights (LOS) associated to two points X_1 and X_2 of the target expressed in the sensor frame, as shown in Figure 4. This corresponds to a distance $\Delta X \geq 0$ on the surface of the target. The relative range between the chaser and the target is assumed to be significantly larger than ΔX . Therefore, the measurement can be approached by $\alpha = \arctan \frac{\Delta X}{r}$ where r is the relative range. The involved uncertainties are the payload sensor resolution ε_α , the evaluation error $\varepsilon_{\Delta X}$ on the ΔX distance, and the navigation range error ε_r . Such uncertainties affect the measurements of the angle α as follows:

$$\hat{\alpha} = \alpha \pm \varepsilon_\alpha = \frac{\Delta X \pm \varepsilon_{\Delta X}}{r \pm \varepsilon_r} \quad (13)$$

which yields:

$$\varepsilon_{\Delta X} \leq r|\varepsilon_\alpha| + |\varepsilon_r| \frac{\Delta X}{r} + |\varepsilon_r||\varepsilon_\alpha| \quad (14)$$

where α is assumed to be small. Assuming that the size of the target is known, the range error r can be related to the relative navigation uncertainty in position. In practice, this can be achieved by considering ε_r as an error bound at $n\hat{\sigma}_p$ on the position components (with, e.g., $n = 3$ and $\hat{\sigma}_p$ the spectral radius of the filter covariance $\hat{\mathbf{P}}_k$ on position components). $\varepsilon_{\Delta X}$ can be taken as a payload performance evaluation.

A similar model can be designed to quantify the velocity evaluation error for a point X of the target. Consider the traveled distance ΔX of X during a time $\Delta t > 0$. The estimated velocity of X in LVLH frame can be expressed as:

$$\hat{v}_x \leq \frac{\Delta X + |\varepsilon_{\Delta X}|}{\Delta t} + (v_x^s + |\varepsilon_v|) + (r + |\varepsilon_r|)(\Omega_z^s + |\varepsilon_\Omega|) \quad (15)$$

where v_x^s is the chaser relative velocity projected to the component x of sensor frame and Ω_z^s is the chaser angular rate projected to the component z of sensor frame. ε_v and ε_Ω can be respectively be linked to relative velocity navigation uncertainty and angular rate noise (gyrometers). An upper bound of the velocity payload performance evaluation criterion ε_{v_x} can then be derived from Eq. (15), for example by taking the worst case for involved uncertainties. The payload cost in Problem (6) can be defined by:

$$\boldsymbol{\varepsilon} = \begin{bmatrix} \varepsilon_{\Delta X} \\ \varepsilon_{v_x} \end{bmatrix} \quad (16)$$

Power budget—Usual constraints on small satellites include the power budget dedicated to each subsystem. Power subsystem is considered to be already designed, providing as input the amount of power available for combined AOCS and payload subsystems. The power budget equation is defined in Eq. (17). Power consumption of devices is taken from the different databases.

$$P(\mathbf{X}) = \sum_{i=1}^N P_{\mathbf{X}[i]} \quad (17)$$

where $P_{\mathbf{X}[i]}$ is the power consumption of device $\mathbf{X}[i]$.

Mass and Volume budgets—Mass is a critical characteristic of satellite conception. Directly related to the cost, it most of the times drives (or at least comes into play for) the key choices of the design process. As for power, the masses of the different devices are extracted from their respective databases. The mass and the volume budget equation are also based on a total sum.

$$M(\mathbf{X}) = \sum_{i=1}^N M_{\mathbf{X}[i]} \quad (18)$$

$$V(\mathbf{X}) = \sum_{i=1}^N V_{\mathbf{X}[i]} \quad (19)$$

where $M_{\mathbf{X}[i]}$ and $V_{\mathbf{X}[i]}$ are the mass and the volume of device $\mathbf{X}[i]$.

4. DATA DESIGN OPTIONS

The MDO process determines the most adequate combination of sensors and actuators from databases to perform on-orbit rendezvous in LEO. In this section, performances and

models of COTS sensors and actuators are presented. In what follows, a unique number is assigned to each sensor to anonymize the brand to which it belongs. Obtained values are taken from datasheets provided by manufacturers.

1. Navigation sensors database

Inertial Measurements Unit (IMU)—Inertial measurements units are widely used devices in the aerospace field to estimate position, velocity and attitude by numerically integrating specific acceleration and angular rate. IMUs are made up of three accelerometers and three gyroscopes. Due to the iterative integration of measurements, the resulting navigation solution is affected by a drifting error. In the present work, twenty-six COTS IMUs are used.

Gyroscope and accelerometer were modeled by Eq. (20). The acceleration γ and the angular rate ω are expressed in the body frame. γ_{true} and ω_{true} correspond to the actual accelerations and angular rates. ξ , v and τ represent the bias, the noise and the scale factor, respectively.

$$\begin{cases} \gamma_{meas} &= \gamma_{true} (1 + \tau_{acc}) + \xi_{acc} + v_{acc} \\ \omega_{meas} &= \omega_{true} (1 + \tau_{gyro}) + \xi_{gyro} + v_{gyro} \end{cases} \quad (20)$$

The following figures illustrate the distribution of IMU performance features within the whole database. Figure 6 and 7 describe the gyroscope bias and the accelerometers bias with respect to the mass of the IMU itself, respectively. These figures highlight the complexity of selecting a sensor from the full device set in an optimal way. Ideally, the selected sensor should have a low bias and a low mass. However, better accuracies are generally obtained with heavier sensors, while low mass sensors can even have two order of magnitude worse performance (e.g. bias). A similar behavior appears with IMU random walks and scale factors. This motivates the use of a global optimization algorithm to find an appropriate trade-off.

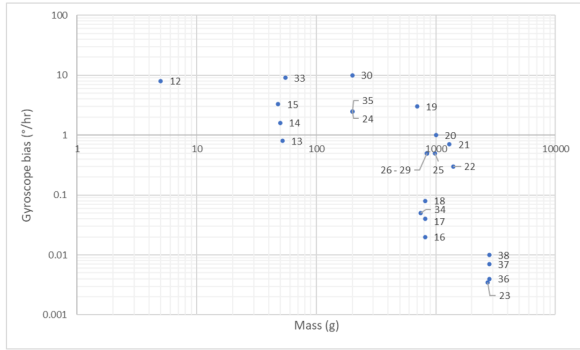


Figure 6: IMU gyroscope: Bias vs. mass

Star sensors—Star sensors aim to determine the attitude of the satellite by matching between optical measurements and an embedded celestial map. In recent years, the use of this type of sensor has increased continuously thanks to its high accuracy range (from 1 to 10 arcsec) [20]. However, the high accuracy of these sensors yields high cost, weight and size, which requires a challenging design trade-off. Forty-three COTS star sensors are considered in the database.

Eq. (21) models the observation equation of the star sensor. The true quaternion q_{true} represents the actual attitude quaternion of the chaser. The star sensor bias ξ_{ST} and noise v_{ST} are

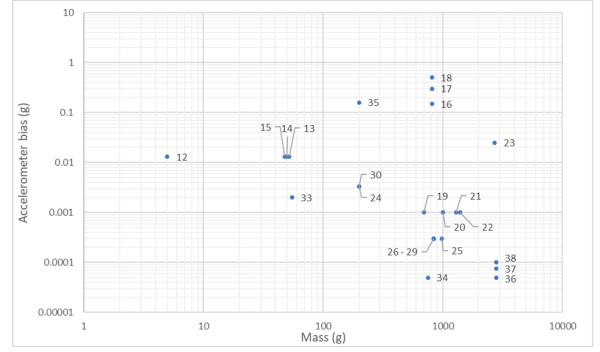


Figure 7: IMU accelerometer: Bias vs. mass

provided by manufacturers. q_ξ and q_v are the quaternions representing the pointing errors due to the bias and random noise of the instrument, respectively.

$$q_{meas} = q_\xi q_v q_{true} \quad (21)$$

Figure 8 and 9 describe the pitch, yaw and roll bias as a function of the mass of the star sensor. As for the IMUs, the relation between accuracy and mass reduction describes the complexity of realizing trade-offs. The large number of star sensors increases the complexity of the selection.

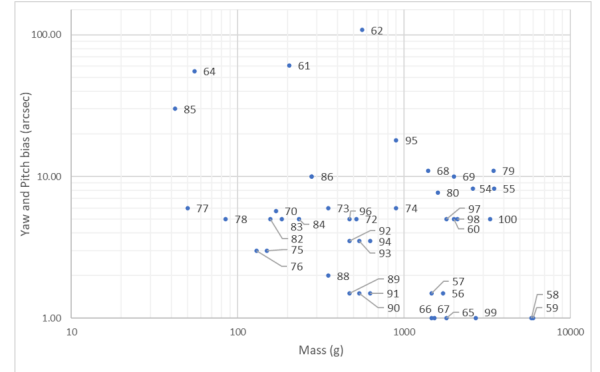


Figure 8: Star sensor: Pitch and yaw bias vs. mass

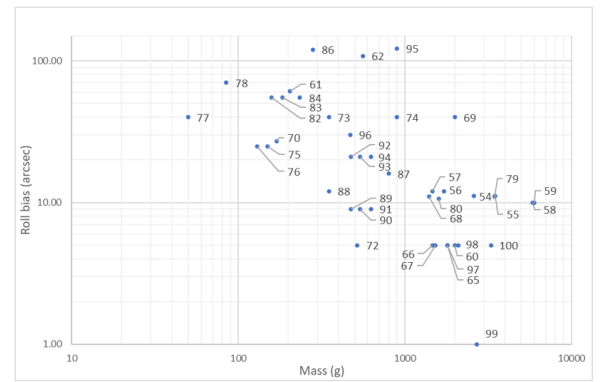


Figure 9: Star sensor: Roll bias vs. mass

LIDARs—LIDARs (Light Detection And Ranging) are using the electromagnetic waves in visible spectrum and near infrared to measure relative position and/or attitude with respect

to another satellite. This technology tends to be used for most rendezvous mission, thanks to its accuracy and depth measurement ability.

In this paper, LIDARs' measurements are modeled as polar relative position data. While δr_l^{meas} describes the distance between the chaser satellite and the target satellite in the LIDAR frame, the line of sight characterizes the angular direction of the target from the chaser point of view. These angles are the elevation θ_l^{true} and the azimuth ϕ_l^{true} of vector δr (Figure 1) in the LIDAR frame.

$$\mathbf{L}_{meas} = \begin{bmatrix} \theta_l^{meas} \\ \phi_l^{meas} \\ \delta r_l^{meas} \end{bmatrix} = \begin{bmatrix} \theta_l^{true} + \xi_l^{ang} + v_l^{ang} \\ \phi_l^{true} + \xi_l^{ang} + v_l^{ang} \\ \delta r_l^{true} + \xi_l^{dist} + v_l^{dist} \end{bmatrix} \quad (22)$$

ξ_l^{ang} , v_l^{ang} , ξ_l^{dist} and v_l^{dist} respectively correspond to the bias and the noise of the LIDAR on the angular measurements (azimuth and elevation) and on the relative distance (range). Eq. (23) describes the conversion from the relative position coordinates to the spherical coordinates.

$$\begin{cases} \theta_l^{meas} &= \arctan\left(\frac{\delta z}{\sqrt{\delta x^2 + \delta y^2}}\right) \\ \phi_l^{meas} &= \arctan\left(\frac{\delta y}{\delta x}\right) \\ \delta r_l^{meas} &= \sqrt{\delta x^2 + \delta y^2 + \delta z^2} \end{cases} \quad (23)$$

Based on open literature, three LIDARs are considered in the database. As the accuracy of LIDARs depends on the distance between the chaser and the target, it was chosen to compare the bias with the mass for a reference range of 100 meters.

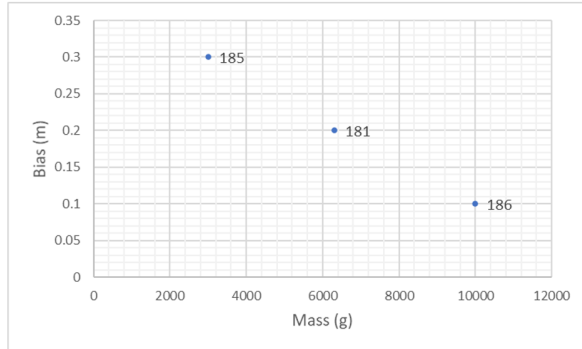


Figure 10: LIDAR: Bias vs. mass at 100 m

2. Payload sensors database

In this study, the considered chaser payload is a camera operating in the visible spectrum directed towards the target satellite. This payload is used to determine the distance on the surface of the target and the velocity of points on the surface of the target. The key drivers impacting the uncertainty of the camera are the field of view (FOV) and the resolution. It was considered that the accuracy of the camera is the mean of the quotient of the FOV on the resolution calculated horizontally and vertically.

Nineteen COTS cameras were listed (see e.g. Figure 11, accuracy as function of the sensor mass).

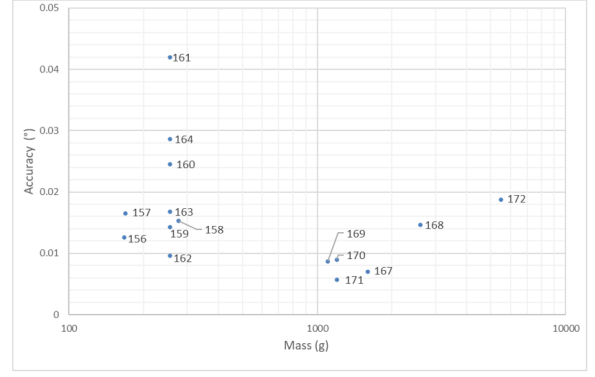


Figure 11: Payload: Accuracy vs. mass

3. Actuators database

Reaction wheels—Reaction wheels are torque motors with integrated rotors that can spin in either direction, providing one axis control per wheel [20]. They are used to slew the spacecraft, i.e. reorienting the vehicle when needed. Wheels most often deal with disturbances and pointing perturbations, to which they respond by spinning at higher speed, creating a torque. In the present work, twenty-six COTS reaction wheels are listed with their mass, power, and performances. Figures 12 and 13 show respectively the torque and the angular momentum of the listed reaction wheels with respect to their mass.

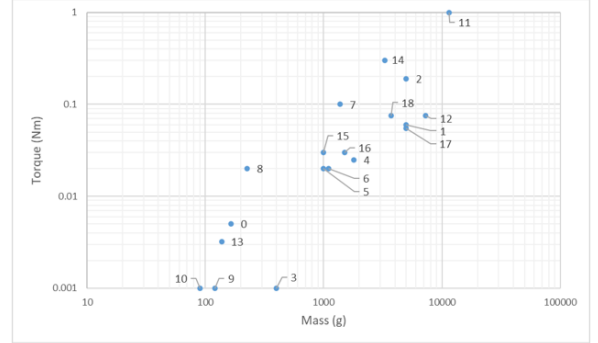


Figure 12: Reaction wheel: Torque vs. mass

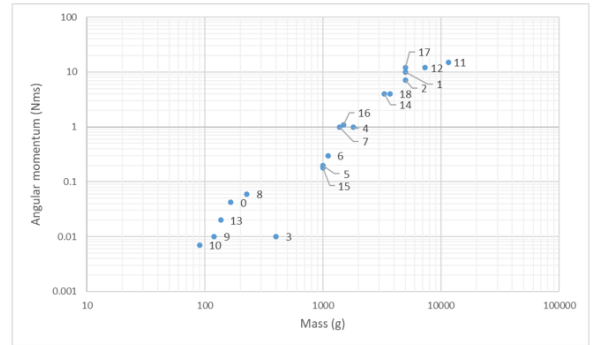


Figure 13: Reaction wheel: Angular momentum vs. mass

Thrusters—In the scope of AOCS subsystem, thrusters are mostly used for orbit maintenance, desaturation of the wheels if required, and for low- Δv maneuvers. The working principle lies in the expulsion of mass which produces a force or a

torque. In the database, eighteen thrusters are listed with their mass, power, Isp and thrust. Two types of thruster were selected, cold gas and monopropellant. Cold gas systems consist of pressurized propellant tank, valves, feed pipes and a nozzle, and provide thrust thanks to the stored enthalpy of the gas. On the opposite, liquid chemical propulsion systems include, as its main parts, a combustion chamber and a convergent-divergent nozzle. These two types of chemical propulsion have the advantage of having excellent flight heritage and are reliable and simple [21]. Figure 14 and 15 show the Isp and the thrust of the listed thrusters with respect to their mass.

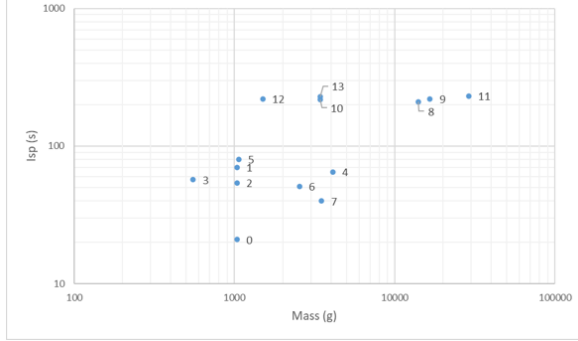


Figure 14: Thruster: Isp vs. mass

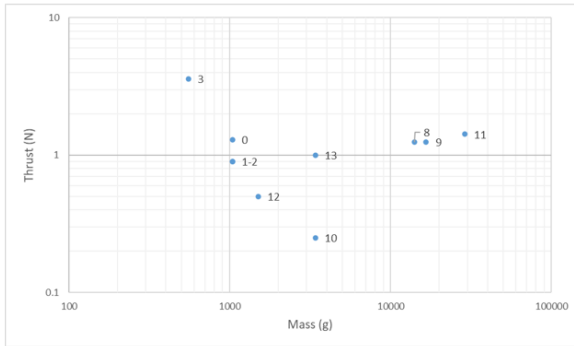


Figure 15: Thruster: Thrust vs. mass

5. TEST CASE

This section presents an application of the proposed methodology to a specific test case scenario. The AVANTI mission [22] is first introduced and a test case trajectory is defined, based on the open literature. MDO results are then provided to illustrate the behavior of the design process on this test-case.

1. AVANTI mission: navigation for non collaborative rendezvous

To assess the method and evaluate the performance of the MDO method, the scenario of the AVANTI mission was selected. In 2016, the German Aerospace Center (DLR) conducted the AVANTI mission that aimed at performing two scenarios between non-cooperative satellites. The first experiment allowed an approach from 13 km to 3 km. The second, an approach from 3 km to 50 m. Both of them were successful [22].

Physics modeling—Two sets of equations are used to model the absolute and relative dynamics of the chaser satellite. Clohessy-Wiltshire equations [13] are used to model the relative translational motion of the chaser with respect to the LVLH reference frame, defined in Section 2-1.

$$\begin{cases} \delta\ddot{x} - 3n^2\delta x - 2n\delta\dot{y} &= u_{ax} \\ \delta\ddot{y} + 2n\delta\dot{x} &= u_{ay} \\ \delta\ddot{z} - n^2\delta z &= u_{az} \end{cases} \quad (24)$$

where n is the mean motion of the chaser satellite and u_{ax} , u_{ay} and u_{az} are the components of the acceleration provided by the thrusters, defined in the LVLH coordinate frame. Angular velocity and quaternion derivatives (respectively $\dot{\boldsymbol{\omega}}$ and $\dot{\mathbf{q}}$) are modeled by the attitude dynamic and kinematic equations (Eq. (25)). $\mathbf{T}_{ext} = \mathbf{T}_{dist} + \mathbf{u}_t$ is the sum of the external torques that are applied on the satellite. This corresponds to the sum of the environmental torques \mathbf{T}_{dist} and of the commanded torques \mathbf{u}_t defined with respect to the body reference frame of the chaser spacecraft. \mathbf{I} is the inertia matrix of the satellite in the body frame. $\boldsymbol{\omega}$ is the angular rate vector of the satellite in the inertial frame and \mathbf{q} the current quaternion.

$$\begin{cases} \dot{\boldsymbol{\omega}} &= \mathbf{I}^{-1} [\mathbf{T}_{ext} - \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega})] \\ \dot{\mathbf{q}} &= \frac{1}{2} \boldsymbol{\Omega} \mathbf{q} \end{cases} \quad (25)$$

with:

$$\boldsymbol{\Omega} = \begin{bmatrix} 0 & \omega_z & -\omega_y & \omega_x \\ -\omega_z & 0 & \omega_x & \omega_y \\ \omega_y & -\omega_x & 0 & \omega_z \\ -\omega_x & -\omega_y & -\omega_z & 0 \end{bmatrix} \quad (26)$$

The two main disturbances acting on the system are the gravity gradient torque \mathbf{T}_{grav} and the aerodynamic drag torque \mathbf{T}_{drag} [23]. Their models are described in Eq. (27). \mathbf{r}_B corresponds to its position in the ECI frame. C_d , A and V are respectively the drag coefficient, the cross sectional area and the velocity of the chaser satellite, respectively. \mathbf{C}_p and \mathbf{C}_m are the position of the center of pressure and the position of the center of mass in the body frame. ρ is the atmospheric density.

$$\begin{cases} \mathbf{T}_{dist} &= \mathbf{T}_{grav} + \mathbf{T}_{drag} \\ \mathbf{T}_{grav} &= 3n^2 \left(\frac{\mathbf{r}_B \times \mathbf{I} \mathbf{r}_B}{r_B^3} \right) \\ \mathbf{T}_{drag} &= \frac{\rho C_d A V^2}{2} \times (\mathbf{C}_p - \mathbf{C}_m) \end{cases} \quad (27)$$

The complete set of equations of motion includes Eq. (24) and Eq. (25) and can be rewritten by adopting a state space representation, where \mathbf{x} is defined as in Eq. (1) and the control actions \mathbf{u} as in Eq. (2). The resulting system can be then rewritten as in Eq. (28). In the following equations, the inertia matrix \mathbf{I} is considered as a diagonal matrix in the body frame.

$$\dot{\mathbf{x}} = \mathbf{F} \mathbf{x} + \mathbf{G} \mathbf{u} + \mathbf{G} \mathbf{T} \quad (28)$$

where:

$$\mathbf{F} = \begin{bmatrix} \mathbf{F}_1 & \mathbf{0}_{6 \times 7} \\ \mathbf{0}_{7 \times 6} & \mathbf{F}_2 \end{bmatrix} \quad \mathbf{G} = \begin{bmatrix} \mathbf{G}_1 & \mathbf{0}_{6 \times 7} \\ \mathbf{0}_{7 \times 6} & \mathbf{G}_2 \end{bmatrix} \quad \mathbf{T} = [\mathbf{0}_{1 \times 6} \quad \mathbf{T}_{dist}^T]^T \quad (29)$$

$$\mathbf{F}_1 = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 3n^2 & 0 & 0 & 0 & 2n & 0 \\ 0 & 0 & 0 & -2n & 0 & 0 \\ 0 & 0 & -n^2 & 1 & 0 & 0 \end{bmatrix} \quad \mathbf{G}_1 = \begin{bmatrix} \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{I}_{3 \times 3} \end{bmatrix} \quad (30)$$

$$\mathbf{F}_2 = \begin{bmatrix} \mathbf{F}_{kin} & \mathbf{0}_{4 \times 3} \\ \mathbf{0}_{3 \times 4} & \mathbf{F}_{dyn} \end{bmatrix} \quad \mathbf{G}_2 = \begin{bmatrix} \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{I}^{-1} \end{bmatrix} \quad (31)$$

$$\mathbf{F}_{kin} = \frac{1}{2} \boldsymbol{\Omega} \quad \mathbf{F}_{dyn} = \frac{1}{2} \begin{bmatrix} 0 & \omega_z \frac{(I_{yy} - I_{zz})}{I_{xx}} & \omega_y \frac{(I_{yy} - I_{zz})}{I_{xx}} \\ \omega_z \frac{(I_{zz} - I_{xx})}{I_{yy}} & 0 & \omega_x \frac{(I_{zz} - I_{xx})}{I_{yy}} \\ \omega_y \frac{(I_{xx} - I_{yy})}{I_{zz}} & \omega_x \frac{(I_{xx} - I_{yy})}{I_{zz}} & 0 \end{bmatrix} \quad (32)$$

Initial conditions and modeled trajectory—The close range rendezvous experiment of the AVANTI mission was chosen as a baseline test case for the simulations [24]. Specifically, the chaser named BIROS is initially placed in a sun-synchronous orbit. The orbital elements of the orbit and relevant physical characteristics of BIROS are described in Table 1 and 2 respectively. The target satellite, BEESAT-4, is launched from BIROS using a picolauncher [25].

Item	Value	Unit
Semi-major axis	6884	km
Eccentricity	0.0012	-
Inclination	97.5	deg
Right ascension of the ascending node	233.6	deg
Argument of perigee	246.3	deg

Table 1: Initial orbital elements

Item	Value	Unit
Volume	$58 \times 88 \times 68$	cm
Mass	140	kg
Ballistic coefficient	$7.9 \cdot 10^{-3}$	$m^2 \cdot kg^{-1}$
Drag coefficient	1.3	-
Inertia matrix	diag(9,6,9)	$kg \cdot m^2$

Table 2: Relevant chaser satellite characteristics

To avoid a collision situation, a spiral-like approach was performed. In this work, we derived a scenario representing a portion of this phase. Initial position and velocity of the chaser, as well as the accelerations, provided during a maneuver were derived from the analysis of [24] and are reported in Figure 16, which shows the results of the Clohessy-Wiltshire equations propagation.

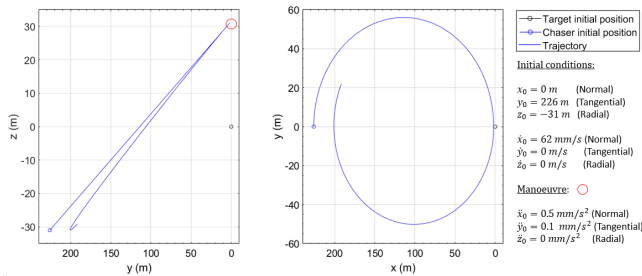


Figure 16: Modelled trajectory

Eq. (33) allows to calculate the initial quaternion from the

initial Direction Cosine Matrix (DCM) \mathbf{R}^0 that describes the rotation from the inertial frame to the body frame.

$$\mathbf{q}_0 = \begin{bmatrix} q_x^0 \\ q_y^0 \\ q_z^0 \\ q_{scalar}^0 \end{bmatrix} = \begin{bmatrix} \frac{1}{4q_{scalar}^0} (\mathbf{R}_{2,3}^0 - \mathbf{R}_{3,2}^0) \\ \frac{1}{4q_{scalar}^0} (\mathbf{R}_{3,1}^0 - \mathbf{R}_{1,3}^0) \\ \frac{1}{4q_{scalar}^0} (\mathbf{R}_{1,2}^0 - \mathbf{R}_{2,1}^0) \\ \frac{1}{2} \sqrt{1 + \mathbf{R}_{1,1}^0 + \mathbf{R}_{2,2}^0 + \mathbf{R}_{3,3}^0} \end{bmatrix} \quad (33)$$

This DCM is calculated thanks to the Eq. (34) where ${}_b\mathbf{R}_{cw}^0$ corresponds to the initial rotation from the body frame to the LVLH frame. It was arbitrarily considered that the x, y and z axes of body frame are respectively aligned with the z, x and y axes of the LVLH frame, respectively. ${}_{cw}\mathbf{R}_i^0$ is computed thanks to the initial position and velocity of the chaser in the inertial frame.

$$\mathbf{R}^0 = {}_b\mathbf{R}_i^0 = {}_b\mathbf{R}_{cw}^0 {}_{cw}\mathbf{R}_i^0 \quad (34)$$

The initial angular rate was set to $[0.05 \ 0 \ 0]^\circ \cdot s^{-1}$.

2. Numerical results

The MDO methodology presented in Section 3-1 is tested on the AVANTI scenario defined in Section 5-1 and the database introduced in Section 4. The design space corresponds to a total of 29,823,768 device configurations (i.e., $18 \times 26 \times 19 \times 3 \times 43 \times 26$).

Optimization's tools definition—To perform the optimization, a Python library called Platypus is used [26]. This library provides optimization algorithms and analysis tools for multiobjective optimization. It includes NSGAII [27], a Non-dominated Sorting Genetic Algorithm II, which is selected to run the simulation.

The visualization of the results is made throughout the utilization of the Pareto front. To explain the reading of this criterion, two usual terms are defined: feasible solution and dominated solution.

A feasible solution is a vector included in the design space, which respects the constraints. A feasible solution \mathbf{a} dominates a feasible solution \mathbf{b} if and only if [28]:

$$\forall i \in [1, \dots, m], F_i(\mathbf{a}) \leq F_i(\mathbf{b}) \quad \text{and} \quad \exists j \in [1, \dots, m], F_j(\mathbf{a}) < F_j(\mathbf{b}) \quad (35)$$

with F the objective function and m the length of a solution vector.

The Pareto front (also called optimal Pareto set) is then the set of the feasible solutions that are non dominated, and can be represented, in the case of a two-objective optimization, with a single two-dimensional plot.

The convergence of the simulation is obtained via the hypervolume indicator. This tool allows to perform quantitative assessment of the Pareto front, by measuring the size of the portion of the objective space that is dominated by the solutions [29]. This measure is made relative to a reference point, ideally far from the Pareto front, from which this portion can be computed.

Represented on Figure 17, the hypervolume $I_H(A)$ of the solution set A can mathematically be defined as the Lebesgue measure λ of the set $H(A, R)$:

$$I_H(A) = \lambda(H(A, R)) = \int_{\mathbb{R}^2} \mathbf{1}_{H(A, R)}(z) dz \quad (36)$$

with :

$$H(A, R) = \{(z_1, z_2) \in \mathbb{R}^2; \exists x \in A, \exists (r_1, r_2) \in R : \forall 1 \leq i \leq 2 : p_i(x) \leq z \leq r_i\} \quad (37)$$

being the set of objective vectors that are enclosed by the Pareto front $p(A)$; $\mathbf{1}_{H(A,R)}$ is the characteristic function of $H(A,R)$; and eventually R is the reference set.

This definition is given in [30], where more information can be found on hypervolume issues.

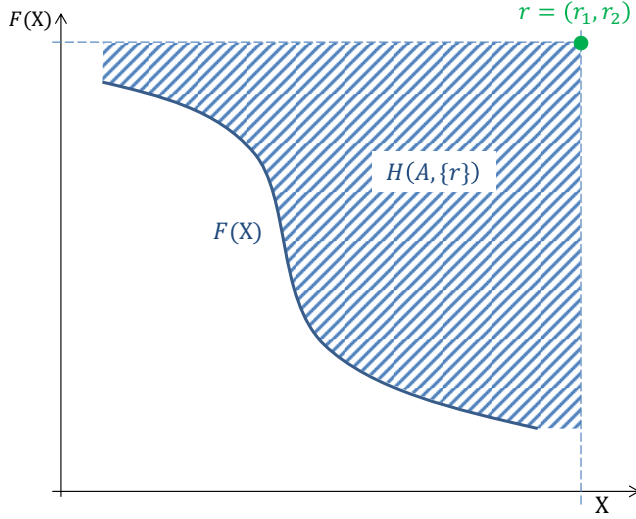


Figure 17: The hypervolume $H(A,R)$ corresponds to the hatched area, between the solution set A (here described by function $F(\mathbf{X})$) and the reference $r = (r_1, r_2)$ [30]. Hypervolume's value increases as the Pareto front gets closer to the origin.

Numerical settings—The values of the different settings and parameters that come into play for this simulation (equations 9 to 12) are as follow:

- The moment arm is evaluated thanks to the satellite dimensions provided in Table 2. Taking the optimum spot to mount the thruster (diagonally) yields a moment arm of $L = 0.5\text{m}$.
- The spinning period t_{spin} in Eq. (11), the burn time t_{burn} in Eq. (10) and the maneuvering time t_{man} are set to $t_{spin} = t_{burn} = t_{man} = 1\text{s}$.
- The fuel consumption for the orbit correction is 1% of the satellite wet mass, meaning a mass ratio of $m_{final}/m_{init} = 1.01$ in Eq. (9).
- The trajectory lasts $t_{acq} = 6000\text{s}$ (Eq. (12)).

Power and volume have been attributed limits, represented by constraints in the process. The power constraint includes all the devices, whereas the volume constraint only takes into account the sensors.

Considering all the previous assumptions on the size and mass of the satellite, we can roughly estimate the typical power that could be available for such a mission, based on data from [20]: for a small satellite of 200W total power consumption, payload and AOCS would account for approximately half of the power consumption. A power constraint of 100W was thus chosen for the simulation. The volume limit is set up to 10000 cm^3 .

Eventually, the population is set to 80 individuals developed over 50 generations (yielding 4000 evaluations).

Results—The Pareto front of the simulation is shown in Figure 18. The two objectives were the minimization of the total mass (payload + AOCS) and the minimization of the AOCS sensors' error. The error of the sensors is represented in Figure 18 as a normalized scalar criterion for the sake of readability, calculated with equation 38.

$$E(\mathbf{X}) = \frac{\sigma_p(\mathbf{X})}{\sigma_{p0}} + \frac{\sigma_v(\mathbf{X})}{\sigma_{v0}} + \frac{\sigma_q(\mathbf{X})}{\sigma_{q0}} \quad (38)$$

where σ_{p0} , σ_{v0} and σ_{q0} are constants corresponding to the smallest values that can be taken by $\sigma_p(\mathbf{X})$, $\sigma_v(\mathbf{X})$ and $\sigma_q(\mathbf{X})$, respectively. As a consequence, $E(\mathbf{X}) \geq 1$.

The resulting design variables configurations of every final solution are also given in Figure 19. LIDAR, reaction wheel and thruster appear to stay the same (i.e only one component for all the solutions), while IMU, star tracker and payload propose more options.

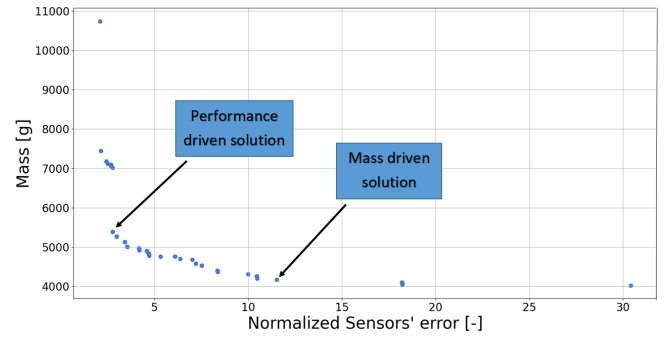


Figure 18: Pareto front resulting from the MDO process. Sensors' error (normalized scalar criterion) is represented along with mass (in grams).

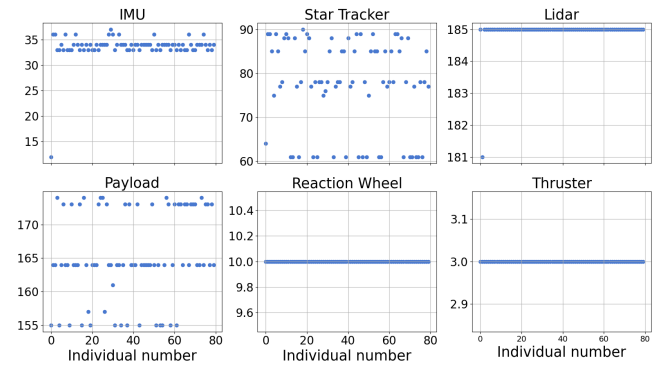


Figure 19: Final values of the design variables. X-axis shows the 80 individuals from the population. Y-axis gives the ID of the different devices.

The hypervolume indicator for this case is shown in Figure 20, and is calculated from the reference point ($E(\mathbf{X}) = 50$, $M(\mathbf{X}) = 60000\text{g}$).

The final values of components ID and of their associated power and volume margin values are presented in Figures 19 and 21.

Just as for power and volume, the margin capacities for the different variables of the actuators are shown. The reading

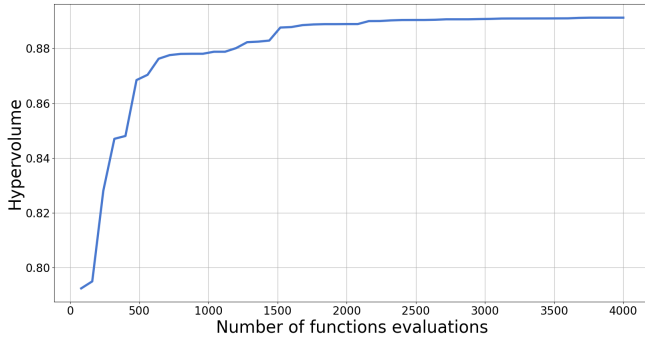


Figure 20: Convergence of simulation represented by Hyper-volume.

of the plots should be like this : a value of 2 on the Y-axis for an individual on, for instance, the torque plot (bottom middle graph on Figure 21) means that this particular devices' configuration has in capacity twice the necessary torque.

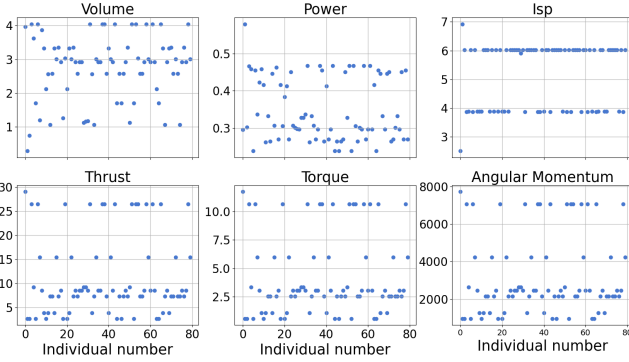


Figure 21: Configurations final values for constraints margins. Along with Power and Volume, we also show the margins left for the actuators capacities.

More than just a unique optimum, the Pareto front outputs a set of optimal solutions. These solutions are best compromises between the two antagonists objectives of mass reduction and performance.

In the present work, equal weight has been given to both inside the objective function: however, it is possible to modify this weight, and value more one over another.

But even in such case, a whole set of optimal solutions is presented to the decision-maker. This leaves the possibility of choice among the solutions, and especially the ability to visually find which one suits the best the needs.

To this extent, two solutions are proposed in this work : one minimizing mass and the other focusing on performance (errors' minimization). They are shown in Figure 18, as mass driven solution and performance driven solution, respectively. Tables 3 and 4 summarizes these two possible combinations of components obtained with MDO.

Within the design space (i.e. all available COTS components), the cost to gain mass (or performance) while still respecting the constraints expands fast when reaching the limits of the design area (Figure 18). Moreover, and as it could be expected, some components have greater influence on the results than others. Choices of actuators stay limited

to fit in the different constraints. On the other hand, sensors and payload offer broader ranges of possibilities. It is worth noting that some components can sometimes have barely the same performances or characteristics, which can cause final values to be shared among those equivalent components.

Component	ID or value
Sensors' error	2.76
Mass	5391g
IMU	34
Star Tracker	89
LIDAR	185
Payload	164
Reaction Wheel	10
Thruster	3

Table 3: First solution of the MDO process : focus on performance

Component	ID or value
Sensors' error	11.5
Mass	4167g
IMU	33
Star Tracker	75
LIDAR	185
Payload	155
Reaction Wheel	10
Thruster	3

Table 4: Second solution of the MDO process : focus on mass

3. Performance of the MDO algorithm

Table 5 presents the navigation performance for two specific sensor configurations.

The best configuration corresponds to the output of an unconstrained optimization (IMU 36, Star Tracker 87, LIDAR 186, Payload 171). The low quality configuration illustrates the impact of low accuracy sensors on navigation performance (IMU 18, Star Tracker 92, LIDAR 185, Payload 155).

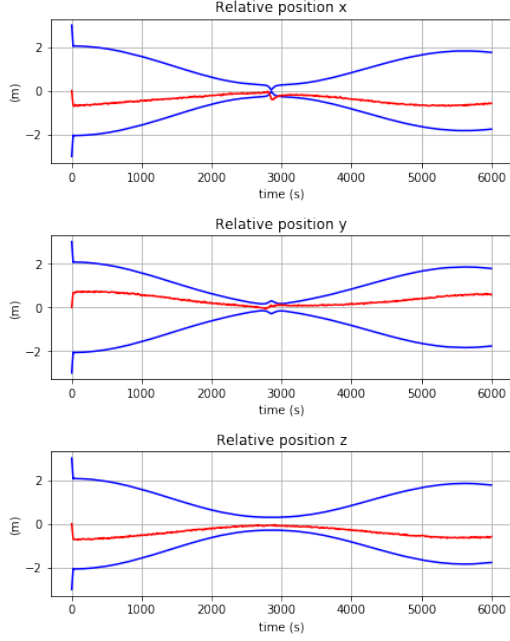
Performance indicators are navigation filter accuracy in relative position σ_p , relative velocity σ_v and attitude σ_q (in terms of navigation filter standard deviation), the payload performance in position detection ϵ_{AX} and velocity evaluation ϵ_{vX} .

A significant impact of the choice of the sensors' configuration can be noticed on all criteria, especially the navigation velocity, which is a critical point for collision avoidance. Since the actual value of relative velocity is about 0.1 m/s, it needs to be estimated with an accuracy of one or two orders of magnitude below.

Figure 22 illustrates the filter's relative position estimation error and covariance during the whole trajectory for two sensor configurations.

Finally, one of the key advantage of MDO is the gain of computational time. Whereas it would have taken the computation of all the 29,823,768 possible devices configurations, only 320,000 (80 individuals for 4000 evaluations) were necessary to reach acceptable convergence and results for the MDO process. This represents a decrease of computational time of 2 orders of magnitude (98%), which is a significant time reduction.

Low quality configuration (position error):



MDO solution output 2 (position error):

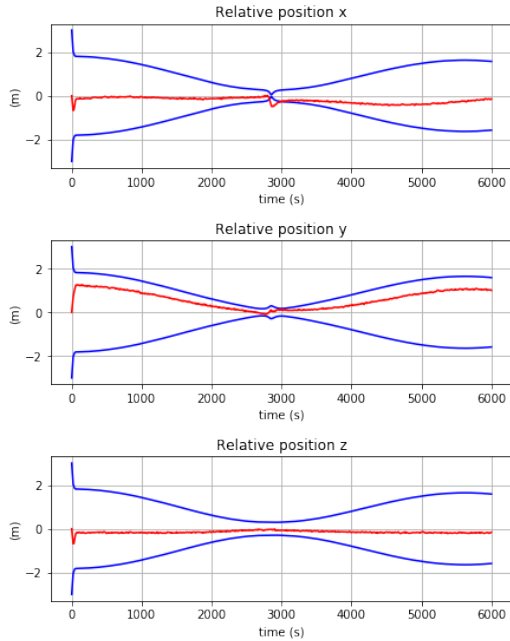


Figure 22: Illustration of the relative position performance for one of the MDO solutions and the low quality configuration. Blue curves represents the filter’s covariance ($\pm 3\sigma$) and red curves plot the filter’s estimation error.

6. CONCLUSION

In this paper, a MDO methodology including navigation sensors choices has been introduced for satellite design in the context of non cooperative rendezvous. The optimization problem is formulated in terms of mass reduction and navigation and payload performance maximization, subject to volume and power consumption constraints. The optimization process is based on a Genetic Algorithm that aims to find the optimal sensors and actuators configuration among

	σ_p (m)	σ_v (m/s)	σ_q	ε_{AX} (m)	ε_{v_x} (m/s)
Best conf.	0.19	0.007	6.23e-6	0.034	0.30
MDO sol. 1	0.39	0.007	1.003e-5	0.12	0.40
MDO sol. 2	0.52	0.080	5.74e-5	0.27	0.80
Low qual. conf.	0.59	15.46	2.62e-5	0.28	46.93

Table 5: Navigation and payload sub-systems performance at final time for four specific sensor configurations. The best configuration corresponds to the output of unconstrained optimization (IMU 36, Star Tracker 87, LIDAR 186, Payload 171). The MDO solutions 1 and 2 respectively correspond to the configurations described in Tables 3 and 4. The low quality configuration corresponds to low accuracy sensors (IMU 18, Star Tracker 92, LIDAR 185, Payload 155).

a COTS device database (e.g., IMU, Star Tracker, LIDAR, Optical camera, reaction wheels, thrusters).

The navigation performance evaluation involves the simulation of the whole navigation chain, including sensor emulation and navigation filter evaluation (e.g. an Extended Kalman Filter). Accounting for the whole navigation chain in the design process is critical in the context of non cooperative rendezvous, since sensor uncertainties are coupled in a nonlinear way. Furthermore, the navigation performance is highly related to the mission success and to the spacecraft safety, as well as the other sub-systems.

The proposed MDO scheme offers the interest of providing not only an optimal solution among a large combinatory of devices, but also a subset of admissible solutions using the Pareto front criterion. This subset of design solutions can be used to orient the work of design engineers as a primary hardware solution selection. The identified design solutions can then be further studied or included in more extensive MDO schemes.

The methodology was applied to the AVANTI mission scenario. Obtained results demonstrate that the proposed MDO process allows for an optimization of the relative navigation equipment while satisfying the spacecraft design constraints.

Future works may involve more extensive design variables, such as other subsystems, trajectory and maneuver optimization, or financial cost minimization. There could be some interest in adapting the algorithm if more subsystems were to be added, such as switching from NSGAI (single-level) to Collaborative Optimization (multi-level) to reduce simulation time.

The proposed approach can be considered as a linchpin to automatize design processes that include recursive estimation algorithms and can be extended to other fields of study such as aeronautics, automotive, medical or mobile robotics.

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REFERENCES

- [1] L. Felicetti, P. Gasbarri, A. Pisculli, M. Sabatini, and G. B. Palmerini, “Design of robotic manipulators for

- orbit removal of spent launchers' stages," *Acta Astronautica*, vol. 119, pp. 118–130, 2016.
- [2] M. Shan, J. Guo, and E. Gill, "Review and comparison of active space debris capturing and removal methods," *Progress in Aerospace Sciences*, vol. 80, pp. 18–32, 2016.
- [3] W. Fehse, "Rendezvous with and Capture / Removal of Non-Cooperative Bodies in Orbit: The Technical Challenges," *Journal of Space Safety Engineering*, vol. 1, no. 1, pp. 17–27, 2014.
- [4] R. Opromolla, G. Fasano, G. Rufino, and M. Grassi, "A review of cooperative and uncooperative spacecraft pose determination techniques for close-proximity operations," *Progress in Aerospace Sciences*, vol. 93, pp. 53–72, 2017.
- [5] J. Sobieszczanski-Sobieski, "Multidisciplinary Design Optimization: An Emerging New Engineering Discipline," pp. 483–496, 1995.
- [6] N. Bérend and S. Bertrand, "MDO approach for early design of aerobraking orbital transfer vehicles," *International Astronautical Federation - 59th International Astronautical Congress 2008, IAC 2008*, vol. 7, pp. 4589–4599, 2008.
- [7] W. Wu, H. Huang, S. Chen, and B. Wu, "Satellite multidisciplinary design optimization with a high-fidelity model," *Journal of Spacecraft and Rockets*, vol. 50, no. 2, pp. 463–467, 2013.
- [8] X. H. Wang, R. J. Li, and R. W. Xia, "Comparison of MDO methods for an earth observation satellite," *Procedia Engineering*, vol. 67, pp. 166–177, 2013.
- [9] J. T. Hwang, D. Y. Lee, J. W. Cutler, and J. R. Martins, "Large-scale MDO of a small satellite using a novel framework for the solution of coupled systems and their derivatives," *Collection of Technical Papers - AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics and Materials Conference*, 2013.
- [10] R. Shi, L. Liu, T. Long, J. Liu, and B. Yuan, "Surrogate assisted multidisciplinary design optimization for an all-electric GEO satellite," *Acta Astronautica*, vol. 138, pp. 301–317, 2017.
- [11] S. Berrezzoug, A. Boudjemai, and F. Bendimerad, "Interactive design and multidisciplinary optimization of geostationary communication satellite," *International Journal on Interactive Design and Manufacturing*, 2019.
- [12] M. Ribeiro, "Kalman and extended kalman filters : concept, derivation and properties," Tech. Rep., 2004.
- [13] H. D. Curtis, *Orbital Mechanics for Engineering Students*, 2013.
- [14] A. Ravanbakhsh, Ph.D. dissertation, Multidisciplinary design Optimization application to conceptual design of university-class microsatellite projects, 2014.
- [15] A. Jafarsalehi, P. M. Zadeh, and M. Mirshams, "Collaborative optimization of remote sensing small satellite mission using genetic algorithms," *Iranian Journal of Science and Technology - Transactions of Mechanical Engineering*, vol. 36, no. M2, pp. 117–128, 2012.
- [16] R. Hassan, B. Cohanin, O. De Weck, and G. Venter, "A comparison of particle swarm optimization and the genetic algorithm," *Collection of Technical Papers - AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics and Materials Conference*, vol. 2, pp. 1138–1150, 2005.
- [17] J.-A. Leal-Naranjo and M. e. a. Ceccarelli, "Multi-objective optimization of a parallel manipulator for the design of a prosthetic arm using genetic algorithms," *Latin American Journal of Solids and Structures*, 2018.
- [18] M. Balesdent, N. Bérend, P. Dépincé, and A. Chriette, "A survey of multidisciplinary design optimization methods in launch vehicle design," *Structural and Multidisciplinary Optimization*, vol. 45, no. 5, pp. 619–642, 2012.
- [19] J. R. Martins and A. B. Lambe, "Multidisciplinary design optimization: A survey of architectures," *AIAA Journal*, vol. 51, no. 9, pp. 2049–2075, 2013.
- [20] J. R. Wertz, D. F. Everett, and J. J. Puschell, *Space Mission Engineering: The New SMAD*. Microcosm, 2011.
- [21] K. V. Mani, "Combined Chemical-Electric Propulsion Design and Hybrid Trajectories for Stand-Alone Deep-Space CubeSats [MARIO]," no. 2020-02-04, p. 19, 2020. [Online]. Available: <http://hdl.handle.net/10589/152157>
- [22] J. S. Ardaens and G. Gaias, "Flight demonstration of spaceborne real-time angles-only navigation to a non-cooperative target in low earth orbit," *Acta Astronautica*, vol. 153, pp. 367–382, 2018.
- [23] B. O. Sunde, "Sensor modelling and attitude determination for micro-satellite," Ph.D. dissertation, Norwegian University of Science and Technology, 2005.
- [24] G. Gaias and J. S. Ardaens, "Flight demonstration of autonomous noncooperative rendezvous in low earth orbit," *Journal of Guidance, Control, and Dynamics*, vol. 41, no. 6, pp. 1337–1354, 2018.
- [25] M. Wermuth and G. Gaias, "Operational Concept of a Picosatellite Release From a Leo," *25th ISSFD*, no. 1, pp. 1–20, 2015.
- [26] D. Hadka, "Platypus-multiobjective optimization in python," 2017.
- [27] K. Deb, A. Pratap, S. Agarwal, and T. Meyarivan, "A fast and elitist multiobjective genetic algorithm: Nsga-ii," *IEEE Transactions on Evolutionary Computation*, vol. 6, no. 2, pp. 182–197, 2002.
- [28] M. Balesdent and L. Brevault, "Multidisciplinary Design Optimization, application to aerospace vehicle design," ONERA, Tech. Rep., 2018.
- [29] L. While, P. Hingston, L. Barone, and S. Huband, "A faster algorithm for calculating hypervolume," *IEEE Transactions on Evolutionary Computation*, vol. 10, no. 1, pp. 29–38, 2006.
- [30] A. Auger, J. Bader, D. Brockhoff, and E. Zitzler, "Theory of the hypervolume indicator : optimal μ -distributions and the choice of the reference point," in *Foundations of Genetic Algorithms*, 2009.

BIOGRAPHY



Clément Rappasse has recently completed his dual degree in Astronautics and Space Engineering at Cranfield University in UK after having studied general engineering at Mines de Douai in France. In 2019, he assisted a Ph.D candidate studying the modeling of cryogenic fluid flows in orbiting satellites tanks at the Von Karman Institute in Belgium.



Nicolas Merlinge received the MSc degree in 2015 from Arts Et Métiers Paris-Tech, and the PhD degree from Coventry University and Université Paris-Saclay in 2018. He is currently a research scientist at ONERA - the French aerospace lab. His research interests include state estimation, system identification, and control for aerospace vehicle design.



Baptiste Agez received the MSc in Astronautics and Space Engineering from Cranfield University (UK) and Centrale Marseille (France) in 2016. He is currently a research engineer on new aerospace vehicle concepts at ONERA - the French aerospace lab. His fields of interest include Multi-Disciplinary Optimization, flight dynamics and space systems design.



Leonard Felicetti is a Lecturer in Space Engineering in Cranfield University (UK). He obtained his Ph.D. and he was a Post-Doc Researcher in Sapienza - University of Rome (Italy). In 2015, he was Honorary Research Associate at University of Glasgow (UK) and then, Associate Senior Lecturer in On-board Space Systems in Luleå University of Technology (Sweden). He joined Cranfield University (UK) in 2019, having active roles on both teaching and research activities in the fields of Guidance, Navigation and Control of space systems, Spacecraft Orbital and Attitude Control Systems, space robotics and space systems design.

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Rappasse, Clément

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